

# Analysis of pointwise completeness and pointwise generacy of descriptor electrical circuits by the use of Drazin inverse of matrices

**Streszczenie.** Pokazano, że każdy deskryptowy obwód elektryczny jest układem o pęku regularnym. Punktowa zupełność i punktowa degeneracja zostały przebadane przy użyciu odwrotności Drazina macierzy. Podano warunki punktowej zupełności i punktowej degeneracji deskryptowych obwodów elektrycznych. Rozważania zilustrowano przykładem de skryptowego obwodu elektrycznego. **Analiza punktowej zupełności i punktowej degeneracji deskryptowych obwodów elektrycznych przy użyciu odwrotności Drazina**

**Abstract.** It is shown that every descriptor electrical circuit is a linear system with regular pencil. The pointwise completeness and pointwise generacy of the descriptor electrical circuits is analyzed by the use of Drazin inverse of matrices. Conditions for the pointwise completeness and pointwise generacy of the descriptor electrical circuits are established and illustrated by an example.

**Słowa kluczowe:** analiza, odwrotność Drazina, punktowa zupełność, punktowa degeneracja..

**Keywords:** Analysis, Drazin inverse, pointwise completeness, pointwise generacy, descriptor, electrical circuit.

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## Introduction

Descriptor (singular) linear systems have been considered in many papers and books [1, 2, 5-8, 11-16, 21-23, 28]. The eigenvalues and invariants assignment by state and output feedbacks have been investigated in [14, 22] and the minimum energy control of descriptor linear systems in [16]. In positive systems inputs, state variables and outputs take only non-negative values [9, 20]. Examples of positive systems are industrial processes involving chemical reactors, heat exchangers and distillation columns, storage systems, compartmental systems, water and atmospheric pollution models. A variety of models having positive linear behavior can be found in engineering, management science, economics, social sciences, biology and medicine, etc. The positive fractional linear systems and some of selected problems in theory of fractional systems have been addressed in monograph [22].

Descriptor standard positive linear systems by the use of Drazin inverse has been addressed in [1, 2, 6, 11-13, 21, 23]. The shuffle algorithm has been applied to checking the positivity of descriptor linear systems in [12]. The stability of positive descriptor systems has been investigated in [28]. Reduction and decomposition of descriptor fractional discrete-time linear systems have been considered in [21]. A new class of descriptor fractional linear discrete-time system has been introduced in [23].

The pointwise completeness and pointwise degeneracy for standard and fractional linear systems have been investigated in [3-5, 10, 17-19, 24-27]. The Drazin inverse of matrices has been applied to find the solutions of the state equations of the fractional descriptor continuous-time linear systems with regular pencils in [13].

In this paper the Drazin inverse of matrices is applied to analysis of pointwise completeness and pointwise generacy of descriptor electrical circuits.

The paper is organized as follows. In section 2 some definitions, lemmas and theorems concerning the descriptor continuous-time linear systems and the Drazin inverse matrices are recalled. The regularity of the descriptor electrical circuits is addressed in section 3. It is shown that every descriptor electrical circuit is a linear system with regular pencil. The pointwise completeness and pointwise generacy of the descriptor electrical circuits is analyzed in section 4. Concluding remarks are given in section 5.

The following notation will be used:  $\mathfrak{R}$  - the set of real numbers,  $\mathfrak{R}^{n \times m}$  - the set of  $n \times m$  real matrices and  $\mathfrak{R}^n = \mathfrak{R}^{n \times 1}$ ,  $\mathfrak{R}_+^{n \times m}$  - the set of  $n \times m$  matrices with nonnegative entries and  $\mathfrak{R}_+^n = \mathfrak{R}_+^{n \times 1}$ ,  $M_n$  - the set of  $n \times n$  Metzler matrices (real matrices with nonnegative off-diagonal entries),  $I_n$  - the  $n \times n$  identity matrix,  $\ker A$  (im  $A$ ) - the kernel (image) of the matrix  $A$ .

## Preliminaries

Consider the autonomous fractional descriptor continuous-time linear system

$$(1) \quad E\dot{x}(t) = Ax(t),$$

where  $x(t) \in \mathfrak{R}^n$  is the state vector,  $E, A \in \mathfrak{R}^{n \times n}$ .

It is assumed that  $\det E = 0$  but the pencil  $(E, A)$  of (1) is regular, i.e.

$$(2) \quad \det[Es - A] \neq 0 \text{ for some } s \in \mathbb{C}$$

where  $\mathbb{C}$  is the field of complex numbers.

Assuming that for some chosen  $c \in \mathbb{C}$ ,  $\det[Ec - A] \neq 0$

and premultiplying (1) by  $[Ec - A]^{-1}$  we obtain

$$(3a) \quad \bar{E}\dot{x}(t) = \bar{A}x(t),$$

where

$$(3b) \quad \bar{E} = [Ec - A]^{-1}E, \quad \bar{A} = [Ec - A]^{-1}A.$$

Note that the equations (2.1) and (2.3a) have the same solution  $x(t)$ .

**Definition 1.** [6, 15] The smallest nonnegative integer  $q$  is called the index of the matrix  $\bar{E} \in \mathfrak{R}^{n \times n}$  if

$$(4) \quad \text{rank } \bar{E}^q = \text{rank } \bar{E}^{q+1}.$$

**Definition 2.** [6, 15] A matrix  $\bar{E}^D$  is called the Drazin inverse of  $\bar{E} \in \mathfrak{R}^{n \times n}$  if it satisfies the conditions

$$(5a) \quad \bar{E}\bar{E}^D = \bar{E}^D\bar{E},$$

$$(5b) \quad \overline{E}^D \overline{E} \overline{E}^D = \overline{E}^D,$$

$$(5c) \quad \overline{E}^D \overline{E}^{q+1} = \overline{E}^q,$$

where  $q$  is the index of  $\overline{E}$  defined by (2.3).

The Drazin inverse  $\overline{E}^D$  of a square matrix  $\overline{E}$  always exists and is unique [6, 15]. If  $\det \overline{E} \neq 0$  then  $\overline{E}^D = \overline{E}^{-1}$ . Some methods for computation of the Drazin inverse are given in [15].

**Lemma 1.** [6, 13, 15] The matrices  $\overline{E}$  and  $\overline{A}$  defined by (5b) satisfy the following equalities

$$(6a) \quad \overline{A} \overline{E} = \overline{E} \overline{A} \quad \text{and} \quad \overline{A}^D \overline{E} = \overline{E} \overline{A}^D, \quad \overline{E}^D \overline{A} = \overline{A} \overline{E}^D, \\ \overline{A}^D \overline{E}^D = \overline{E}^D \overline{A}^D,$$

$$(6b) \quad \ker \overline{A} \cap \ker \overline{E} = \{0\},$$

$$(6c) \quad \overline{E} = T \begin{bmatrix} J & 0 \\ 0 & N \end{bmatrix} T^{-1}, \quad \overline{E}^D = T \begin{bmatrix} J^{-1} & 0 \\ 0 & 0 \end{bmatrix} T^{-1},$$

$\det T \neq 0$ ,  $J \in \mathfrak{R}^{n_1 \times n_1}$ , is nonsingular,  $N \in \mathfrak{R}^{n_2 \times n_2}$  is nilpotent,  $n_1 + n_2 = n$ ,

$$(6d) \quad (I_n - \overline{E} \overline{E}^D) \overline{A} \overline{A}^D = I_n - \overline{E} \overline{E}^D \quad \text{and} \\ (I_n - \overline{E} \overline{E}^D) (\overline{E} \overline{A}^D)^q = 0.$$

**Theorem 1.** [13] The solution to the equation (1) is given by

$$(7) \quad x(t) = e^{\overline{E}^D \overline{A} t} \overline{E} \overline{E}^D w,$$

where  $w \in \mathfrak{R}^n$  is arbitrary.

From (7) we have

$$(8) \quad x(0) = x_0 = \overline{E} \overline{E}^D w$$

and

$$(9) \quad x_0 \in \text{im}(\overline{E} \overline{E}^D)$$

where  $\text{im}$  denotes the image of  $\overline{E} \overline{E}^D$ .

**Theorem 2.** Let

$$(10) \quad P = \overline{E} \overline{E}^D \quad \text{and} \quad Q = \overline{E}^D \overline{A}.$$

Then:

$$(11a) \quad P^k = P \quad \text{for } k = 2, 3, \dots,$$

$$(11b) \quad PQ = QP = Q,$$

$$(11c) \quad P \Phi_0(t) = \Phi_0(t).$$

Proof is given in [13].

### Regularity of descriptor linear electrical circuits

Consider the electrical circuits composed of resistors, condensators, coils and voltage (current) sources. It is well-known that such electrical circuits are described by the equation (1) if as the state variables (components of the state vector  $x$ ) the voltages on the condensators and currents in the coils are chosen [15, 22]. In this section it will be shown that the descriptor electrical circuit are linear systems with regular pencils.

**Theorem 3.** Every electrical circuit is a descriptor system if it contains at least one mesh consisting with only ideal capacitors and voltage sources or at least one node with branches with coils.

**Proof.** If the electrical circuit contains at least one mesh consisting of branches with ideal capacitors and voltage sources then the rows of the matrix  $E$  corresponding to the

meshes are zero rows and the matrix  $E$  is singular. If the electrical circuit contains at least one node with branches with coils then the equations written on Kirchhoff's current law for these nodes are algebraic ones and the corresponding rows of  $E$  are zero rows and it is singular.  $\square$

**Theorem 4.** Every descriptor electrical circuit is a linear system with regular pencil.

**Proof.** It is well-known [15, 22] that for a descriptor electrical circuit with  $n$  branches and  $q$  nodes using current Kirchhoff's law we can write  $q - 1$  algebraic equations and the voltage Kirchhoff's law  $n - q + 1$  differential equations. The equalities are linearly independent and can be written in the form (1). From linear independence of the equations it follows that the condition (2) is satisfied and the pencil of the electrical circuit is regular.

**Example 1.** Consider the descriptor electrical circuit shown in Fig. 1 with given resistances  $R_1, R_2, R_3$ ; inductances  $L_1, L_2, L_3$  and source voltages  $e_1$  and  $e_2$ .

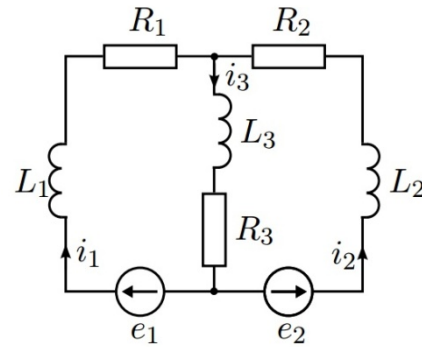


Fig. 1. Electrical circuit of Example 1.

Using Kirchhoff's laws we can write the equations

$$(12a) \quad e_1 = R_1 i_1 + L_1 \frac{di_1}{dt} + R_3 i_3 + L_3 \frac{di_3}{dt}$$

$$(12b) \quad e_2 = R_2 i_2 + L_2 \frac{di_2}{dt} + R_3 i_3 + L_3 \frac{di_3}{dt}$$

$$(12c) \quad 0 = i_1 + i_2 - i_3$$

The equations (3.1) can be written in the form (1), where

$$(13) \quad x = \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix}, \quad u = \begin{bmatrix} e_1 \\ e_2 \end{bmatrix}, \quad E = \begin{bmatrix} L_1 & 0 & L_3 \\ 0 & L_2 & L_3 \\ 0 & 0 & 0 \end{bmatrix},$$

$$A = \begin{bmatrix} -R_1 & 0 & -R_3 \\ 0 & -R_2 & -R_3 \\ 1 & 1 & -1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}.$$

The assumption (2) for the electrical circuit is satisfied, since

$$(14) \quad \det E = \begin{vmatrix} L_1 & 0 & L_3 \\ 0 & L_2 & L_3 \\ 0 & 0 & 0 \end{vmatrix} = 0$$

and

$$\det[Es - A] = \begin{vmatrix} L_1s + R_1 & 0 & L_3s + R_3 \\ 0 & L_2s + R_2 & L_3s + R_3 \\ -1 & -1 & 1 \end{vmatrix}$$

$$= [L_1(L_2 + L_3) + L_2L_3]s^2 + [R_1(L_2 + L_3) + R_2(L_1 + L_3) + R_3(L_1 + L_2)]s + R_1(R_2 + R_3) + R_2R_3$$

(15)

Therefore, the electrical circuit is a descriptor system with regular pencil.

#### 4. Pointwise completeness and pointwise degeneracy

Consider the descriptor linear electrical circuits composed of resistors condensators, coils and voltage (current) source described by the equation (1) for  $u(t) = 0$ ,  $t \geq 0$ .

**Definition 3.** The descriptor electrical circuit (1) (for  $u(t) = 0$ ,  $t \geq 0$ ) is called pointwise complete for  $t = t_f$  if for every final state  $x_f \in \mathfrak{R}^n$  belonging to the set

$$(16) \quad x_f \in \text{im}[e^{\bar{E}^D \bar{A} t_f} x_0]$$

there exists a vector of initial conditions  $x_0 \in \text{im}[\bar{E}\bar{E}^D] \in X_0$  such that  $x(t_f) = x_f \in X_f$ .

**Remark 1.** In general case the set of initial conditions  $X_0$  and the set of final state  $X_f$  are different. For example, if

$$X_0 = \text{im} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \text{ and } e^{\bar{E}^D \bar{A} t} = \begin{bmatrix} 0 & a_{12}(t) \\ a_{21}(t) & a_{22}(t) \end{bmatrix}, \quad a_{12}(t)a_{21}(t) \neq 0,$$

$t \geq 0$  then by (16) we obtain  $X_f = \text{im} \begin{bmatrix} 0 \\ a_{21}(t) \end{bmatrix}$ .

Note that the initial state  $x_0$  and the final state  $x_f$  of the descriptor electrical circuits satisfy the equations written by the use of the Kirchhoff's laws.

**Theorem 5.** The descriptor electrical circuit (1) is pointwise complete for any  $t = t_f$  and every final state  $x_f \in \mathfrak{R}^n$  satisfying (1).

**Proof.** Substituting in (7)  $t = t_f$  we obtain

$$(17) \quad x_f = e^{\bar{E}^D \bar{A} t_f} x_0$$

and

$$(18) \quad x_0 = e^{-\bar{E}^D \bar{A} t_f} x_f \in \text{im}[\bar{E}\bar{E}^D]$$

since the matrix  $e^{\bar{E}^D \bar{A} t_f}$  is nonsingular for any matrix  $\bar{E}^D \bar{A}$ ,  $t_f \geq 0$ .  $\square$

**Definition 4.2.** The descriptor electrical circuit (1) (for  $u(t) = 0$ ,  $t \geq 0$ ) is called pointwise degenerated in the direction  $v$  for  $t = t_f$  if there exists a nonzero vector  $v \in \mathfrak{R}^n$

such that for all initial conditions  $x_0 \in \text{im}[\bar{E}\bar{E}^D]$  the solution of (1) satisfy the condition

$$(19) \quad v^T x_f = 0$$

where  $T$  denotes the transpose.

**Theorem 6.** The descriptor electrical circuit (1) is pointwise degenerated in the direction  $v$  defined by

$$(20) \quad v^T \bar{E} = 0$$

for any  $t_f \geq 0$  and all initial conditions  $x_0 \in \text{im}[\bar{E}\bar{E}^D]$ .

**Proof.** Postmultiplying (20) by  $\bar{E}^D w$  and using  $x_0 = \bar{E}\bar{E}^D w$  and (19) we obtain

$$(21) \quad v^T \bar{E}\bar{E}^D w = v^T x_0 = 0.$$

Taking into account

$$(22) \quad e^{\bar{E}^D \bar{A} t_f} = \sum_{k=0}^{\infty} \frac{(\bar{E}^D \bar{A} t_f)^k}{k!}$$

and (17) we obtain

$$(23) \quad v^T x_f = v^T \left[ \bar{E}\bar{E}^D \bar{A} w + \sum_{k=1}^{\infty} \frac{(\bar{E}^D \bar{A} t_f)^k}{k!} \bar{E}\bar{E}^D \bar{A} w \right]$$

$$= v^T \bar{E} \left[ \bar{E}^D \bar{A} w + \sum_{k=1}^{\infty} \frac{(\bar{E}^D \bar{A} t_f)^k}{k!} \bar{E}^D \bar{A} w \right] = 0$$

since (8) and (20) hold.  $\square$

From (20) and (21) for any  $t_f$  we have the following conclusion.

**Conclusion 1.** The state vector  $x(t)$  of the descriptor electrical circuit satisfies the condition

$$(24) \quad v^T x(t) = 0$$

for  $t \geq 0$ .

**Example 2.** (Continuation of Example 1) Substituting (12) into (14) we obtain

$$(25) \quad E = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 1 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} -1 & 0 & -1 \\ 0 & -1 & -1 \\ 1 & 1 & -1 \end{bmatrix}.$$

The matrix  $A$  given by (25) is nonsingular and we choose  $c = 0$  and we obtain

$$(26a) \quad \bar{E} = [Ec - A]^{-1} E = [-A]^{-1} E$$

$$= \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 1 \\ -1 & -1 & 1 \end{bmatrix}^{-1} \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 1 \\ 0 & 0 & 0 \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 2 & -1 & 1 \\ -1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix},$$

$$(26b) \quad \bar{A} = [Ec - A]^{-1} A = [-A]^{-1} A = - \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

To compute the Drazin inverse of (26) we use the Procedure A.1 (given in Appendix).

Step 1. Using (26a) and (A.1) we obtain

$$(27a) \quad \bar{E} = VW$$

where

$$(27b) \quad V = \frac{1}{3} \begin{bmatrix} 2 & -1 \\ -1 & 2 \\ 1 & 1 \end{bmatrix}, \quad W = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 1 \end{bmatrix}.$$

Step 2. From (A.2), (26a) and (27b) we have

$$(28) \quad W\bar{E}V = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 1 \end{bmatrix} \frac{1}{3} \begin{bmatrix} 2 & -1 & 1 \\ -1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix} \frac{1}{3} \begin{bmatrix} 2 & -1 \\ -1 & 2 \\ 1 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}.$$

Step 3. Using (A.3), (27b) and (28) we obtain

$$(29) \quad \bar{E}^D = V[W\bar{E}V]^{-1}W = VW = \bar{E} = \frac{1}{3} \begin{bmatrix} 2 & -1 & 1 \\ -1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix}.$$

From (29) and (26b) we have

$$(30) \quad \bar{E}^D \bar{A} = \frac{1}{3} \begin{bmatrix} -2 & 1 & -1 \\ 1 & -2 & -1 \\ -1 & -1 & -2 \end{bmatrix}$$

and the characteristic polynomial of (30) has the form

$$(31) \quad \det[I_3 s - \bar{E}^D \bar{A}] = \begin{vmatrix} s + \frac{2}{3} & -\frac{1}{3} & \frac{1}{3} \\ -\frac{1}{3} & s + \frac{2}{3} & \frac{1}{3} \\ \frac{1}{3} & \frac{1}{3} & s + \frac{2}{3} \end{vmatrix} = s^3 + 2s^2 + s$$

and its zeros are  $s_1 = s_2 = -1$ ,  $s_3 = 0$ .

Note that the characteristic polynomial of the pair (25) has the form

$$(32) \quad \det[Es - A] = \begin{vmatrix} s+1 & 0 & s+1 \\ 0 & s+1 & s+1 \\ -1 & -1 & 1 \end{vmatrix} = 3(s^2 + 2s + 1)$$

has the same zeros  $s_1 = s_2 = -1$ ,  $s_3 = 0$ .

Using the Sylvester formula [15] and (4.15) we obtain

$$(33) \quad e^{\bar{E}^D \bar{A} t} = \frac{1}{3} \begin{bmatrix} 2e^{-t} + 1 & 1 - e^{-t} & e^{-t} - 1 \\ 1 - e^{-t} & 2e^{-t} + 1 & e^{-t} - 1 \\ e^{-t} - 1 & e^{-t} - 1 & 2e^{-t} + 1 \end{bmatrix}.$$

From (21) and (26a) we have

$$(34) \quad v^T \bar{E} = [v_1 \quad v_2 \quad v_3] \frac{1}{3} \begin{bmatrix} 2 & -1 & 1 \\ -1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix} \\ = \frac{1}{3} [2v_1 - v_2 + v_3 \quad 2v_2 - v_1 + v_3 \quad 2v_3 + v_1 + v_2] \\ = [0 \quad 0 \quad 0]$$

and  $v^T = [1 \quad 1 \quad -1]$ .

The set of admissible initial conditions is

$$(35) \quad X_0 = \text{im}[\bar{E}\bar{E}^D] = \frac{1}{3} \begin{bmatrix} 2 & -1 & 1 \\ -1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} \\ = \frac{1}{3} \begin{bmatrix} 2a_1 - a_2 + a_3 \\ 2a_2 - a_1 + a_3 \\ 2a_3 + a_1 + a_2 \end{bmatrix}$$

for arbitrary  $a_k$   $k=1,2,3$ , i.e.  $x_0 \in X_0$ .

Note that the admissible initial conditions satisfy the equation (21) since

$2a_1 - a_2 + a_3 + 2a_2 - a_1 + a_3 - (2a_3 + a_1 + a_2) = 0$  for any values of  $a_1, a_2$  and  $a_3$ .

From (17) and (33) we have

$$(36) \quad x_f = e^{\bar{E}^D \bar{A} t_f} x_0 = \frac{1}{3} \begin{bmatrix} 2e^{-t_f} + 1 & 1 - e^{-t_f} & e^{-t_f} - 1 \\ 1 - e^{-t_f} & 2e^{-t_f} + 1 & e^{-t_f} - 1 \\ e^{-t_f} - 1 & e^{-t_f} - 1 & 2e^{-t_f} + 1 \end{bmatrix} \begin{bmatrix} x_{10} \\ x_{20} \\ x_{30} \end{bmatrix} \\ = \begin{bmatrix} (2x_{10} - x_{20} + x_{30})e^{-t_f} \\ (2x_{20} - x_{10} + x_{30})e^{-t_f} \\ (2x_{03} + x_{10} + x_{20})e^{-t_f} \end{bmatrix}$$

since by (35)  $x_{10} + x_{20} - x_{30} = 0$ .

Taking into account (36) and  $v^T = [1 \quad 1 \quad -1]$  it is easy to

check that  $v^T x_f = 0$  for any admissible initial conditions belonging to the set (35).

The descriptor electrical circuit is pointwise completeness for any  $t_f$  and  $x_f$  given by (36) and is pointwise degenerated in the direction  $v^T = [1 \quad 1 \quad -1]$ .

### Concluding remarks

The Drazin inverse of matrices has been applied to analysis of the regularity pointwise completeness and the pointwise generacy of descriptor electrical circuits composed of resistors, condensators, coils and voltage (current) sources. It has been shown that such electrical circuits are descriptor continuous-time linear system with regular pencils (Theorem 4). Conditions for the pointwise completeness and pointwise generacy have been established (Theorem 5 and 6). The considerations have been illustrated by simple descriptor electrical circuit. The considerations can be extended to the fractional descriptor electrical circuits.

### Appendix

#### Procedure for computation of Drazin inverse matrices

To compute the Drazin inverse  $\bar{E}^D$  of the matrix  $\bar{E} \in \mathfrak{R}^{n \times n}$  defined by (3b) the following procedure is recommended.

#### Procedure A.1.

Step 1. Find the pair of matrices  $V \in \mathfrak{R}^{n \times r}$ ,  $W \in \mathfrak{R}^{r \times n}$  such that

$$(A.1) \quad \bar{E} = VW, \quad \text{rank } V = \text{rank } W = \text{rank } \bar{E} = r.$$

As the  $r$  columns (rows) of the matrix  $V$  ( $W$ ) the  $r$  linearly independent columns (rows) of the matrix  $\bar{E}$  can be chosen.

Step 2. Compute the nonsingular matrix

$$(A.2) \quad W\bar{E}V \in \mathfrak{R}^{r \times r}.$$

Step 3. The desired Drazin inverse matrix is given by

$$(A.3) \quad \bar{E}^D = V[W\bar{E}V]^{-1}W.$$

**Proof.** It will be shown that the matrix (A.3) satisfies the three conditions (7) of Definition 2. Taking into account that  $\det WN \neq 0$  and (A.1) we obtain

$$(A.4) \quad [W\bar{E}V]^{-1} = [WVWV]^{-1} = [WV]^{-1}[WV]^{-1}.$$

Using (7a), (A.1) and (A.4) we obtain

$$(A.5a) \quad \begin{aligned} \bar{E}\bar{E}^D &= VWV[W\bar{E}V]^{-1}W = VWV[WV]^{-1}[WV]^{-1}W \\ &= V[WV]^{-1}W \end{aligned}$$

and

$$(A.5b) \quad \begin{aligned} \bar{E}^D\bar{E} &= V[W\bar{E}V]^{-1}WVW \\ &= V[WV]^{-1}[WV]^{-1}WVW = V[WV]^{-1}W. \end{aligned}$$

Therefore, the condition (5a) is satisfied. To check the condition (5b) we compute

$$(A.6) \quad \begin{aligned} \bar{E}^D\bar{E}\bar{E}^D &= V[W\bar{E}V]^{-1}WVWV[W\bar{E}V]^{-1}W \\ &= V[WVWV]^{-1}WVWV[W\bar{E}V]^{-1}W \\ &= V[W\bar{E}V]^{-1}W = \bar{E}^D. \end{aligned}$$

Therefore, the condition (7b) is also satisfied. Using (5c), (A.1), (A.3) and (A.4) we obtain

$$(A.7) \quad \begin{aligned} \bar{E}^D\bar{E}^{q+1} &= V[W\bar{E}V]^{-1}W(VW)^{q+1} \\ &= V[WV]^{-1}[WV]^{-1}WVW^qW^{q+1} \\ &= V[WV]^{-1}V^qW^{q+1} = VW^{q-1}W^q = (VW)^q = \bar{E}^q \end{aligned}$$

where  $q$  is the index of  $\bar{E}$ .

Therefore, the condition (5c) is also satisfied.

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