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Sensor for analysis of engine knock control system

Streszczenie. Niniejszy artykuł dotyczy zjawiska niepożądanego spalania detonacyjnego w silnikach spalinowych. Jednostka sterująca silnika monitoruje te detonacje używając piezoelektrycznych czujników. Dzięki kontroli czujnikami spalania stukowego detonacje mogą być obiektywnie zmierzone po prostu na zewnątrz samochodu. Jeśli ten komponent zapewni małą amplitudą napięcia wyjściowego mogłoby się zdarzyć, że w obszarze zapłonu silnika wystąpiłoby spalanie. Artykuł dotyczy konstrukcji prostego urządzenia do wykrywania tego zaburzenia. (Czujnik do analizy systemu kontrolnego spalania stukowego)

Abstract. This paper deals with the phenomenon of the undesirable detonation combustion in internal combustion engines. A control unit of the engine monitors these detonations using piezoelectric knock sensors. With the control of these sensors the detonations can be objectively measured just outside the car. If this component provides small amplitude of the output voltage it could happen that there would have been in the areas of the engine ignition combustion. The paper deals with design of a simple device for the detection of this disorder.

Słowa kluczowe: czujniki spalania stukowego; diagnostyka; urządzenie do kontroli.
Keywords: knock sensor; diagnostic; testing device.

Introduction

A knock sensor allows the engine to run with the ignition tim-ing as far advanced as possible. The computer will continue to advance the timing until the knock sensor detects pinging. At that point the computer retards the ignition timing just enough for stop the pinging.

The knock sensor responds to the spark knock caused by pre-detonation of the air/fuel mixture. As the flame front moves out from the spark plug ignition point, pressure waves in the chamber crash into the piston or cylinder walls resulting in a sound known as a knock or ping. This is caused by using a fuel with a low octane rating, overheating, or over advanced timing. Sometimes it can be caused by hot carbon deposits on the piston or cylinder head that raise compression. A knock sensor is comprised of piezoelectric materials; crystals that when impacted, generate a voltage (same idea as a BBQ ignitor). This voltage is monitored by the computer, and when an irregularity is detected, the computer corrects timing in VVT (variable valve timing) engines, or triggers a DTC Diagnostic Trouble Code) in older vehicles. [1-3].

Fig.1. Bandpass output signal: *a*) non-knocking combustion, *b*) knocking combustion [1]

Engine Knocking

Detonation can be prevented by any or all of the following techniques:
- the use of a fuel with high octane rating, which increases the combustion temperature of the fuel and reduces the proclivity to detonate;
- enriching the air-fuel ratio which alters the chemical reactions during combustion, reduces the combustion temperature and increases the margin above detonation;
- reducing peak cylinder pressure by decreasing the engine revolutions (e.g., shifting to a higher gear, there is also evidence that knock occurs more easily at high rpm than low regardless of other factors);
- decreasing the manifold pressure by reducing the throttle opening, boost pressure or
- reducing the load on the engine.

At detonation combustion occurs to rapid changes in pressure (Fig.1). These fast pressure changes, generated by sound waves, which are in modern automobiles captured by the knock sensor [4].

Adaptive Knock Control

At dynamic engine transients, mismatches of the ignition angle occur resulting in increased knock occurrence rates. The response time of knock control can be reduced by a feed-forward control angle $\alpha_l(n)$ stored in an adaptive ignition angle map. Contrary to lambda control, a successful global error model has not yet been found. The values of the ignition angle map must therefore be adapted in every individual engine operating point for all cylinders.

The ignition angle at one cylinder is the sum:

$$(1) \qquad \alpha_e(n) = \alpha_i(n) + \alpha_k(n) + \alpha_l(n),$$

where α_e is the effective ignition angle, α_i is the open loop ignition angle from fixed map, α_k is the knock control ignition angle, and α_l is the learned ignition angle from adaptive map.

The average knock control ignition angle $\alpha_k(n)$ is the basis to teach the adaptive ignition angle map $\alpha_l(n)$ into the direction of retarding. A figed advance angle αa is superimposed to the teaching process providing a forgetting function of the thought angles. The learned ignition angle is

$$(2) \quad \alpha_l(n) = (1 - k_l)\alpha_l(n-1) + k_l\left(\overline{\alpha}_k(n-1) + \alpha_a(n-1)\right).$$

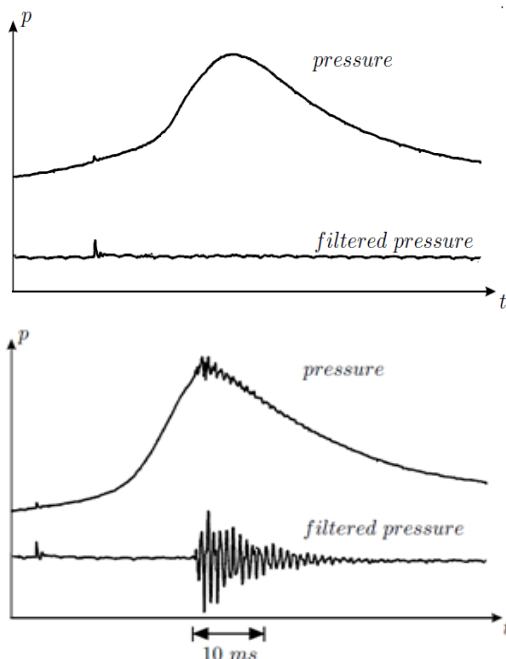The factor k_l determines how fast the learning process is [5].

The ilustration of knock control with feed-forward adaptive ignition angle map is shown on Fig.2.
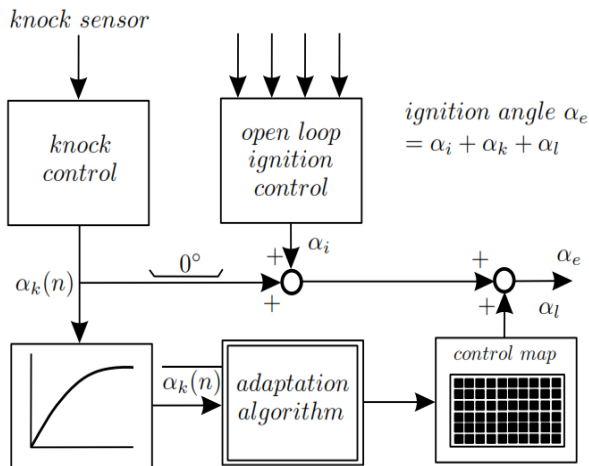

Fig.2. Knock control with feed-forward adaptive ignition angle map [5]

The usual actuation is a retardation of the ignition angle, shifting the energy conversion process backwards and thus reducing peak pressures and teperatures. An alternative input may be to lower the boost pressure of a turbo charger. The knock control ignition angle is calculated at discrete combustion cycles n as

$$(3) \qquad \alpha_k(n) = \alpha_k(n-1) + \Delta\alpha_k - \beta \cdot \Delta E_y(n)$$

where $\Delta\alpha_k$ is a permanent ignistion angle advance, and $\beta\Delta E_y(n)$ the ignition angle retard at knocking. A typical control cycle is shown in Fig.3. The knock control ignition angle $\alpha_k(n)$ is added to the ignition angle obtained from the ignition map.
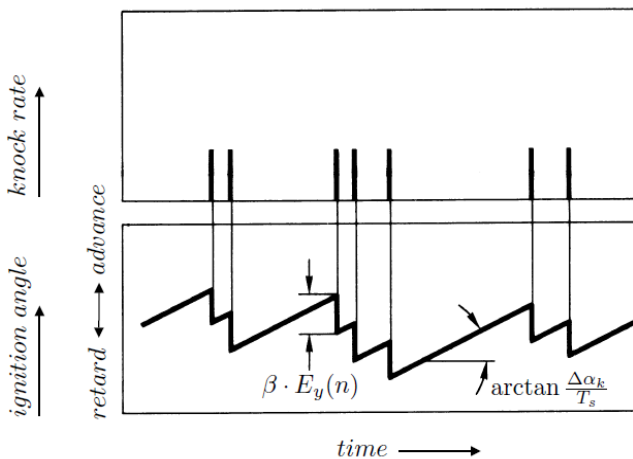

Fig.3. Control of knock occurrence rate by ignition angle shifting [5]

Knock Sensor Output Signal
Sound waves generated by detonation during combustion have a frequency of between 6 to 20 kHz. Their frequency can be approximated by:

$$(4) \qquad f_{mn} = c_0 \sqrt{v/273\mathbf{K}} \cdot \beta_{mn}/d \,,$$

where c_0 is the sound propagation velocity at 273 K, v is the temperature within combustion chamber, d is the cylinder diameter, β_{mn} is the Bessel function (e.g. β_{10}=0.5861, β_{20}=0.9722, β_{30}=1.2197).
From the parameters c_0 = 330 m/s, v = 2500 K, d = 0.089 m we can calculate the knock resonance

frequencies f_{10}= 6.6 kHz, f_{20} = 10.9 kHz, f_{30}= 13.7 kHz.
Bessel functions are defined as the solutions $y(x)$ of Bessel's differential equation:

$$(5) \quad x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} + \left(x^2 - a^2\right)y = 0 \,.$$

It is possible to define the function by its Taylor series expansion around x = 0:

$$(6) \quad J_\alpha(x) = \sum_{n=0}^{\infty} \frac{(-1)^m}{m!\,\Gamma(m + \alpha + 1)}\left(\frac{x}{2}\right)^{2m+\alpha} .$$

where Γ is the gamma function, a shifted generalization of the factorial function to non-integer values.
The Bessel function of the first kind is an entire function if α is an integer (Fig.4). The graphs of Bessel functions look roughly like oscillating sine or cosine functions that decay proportionally to $1/\sqrt{x}$ (see also their asymptotic forms below), although their roots are not generally periodic, except asymptotically for large x [6].
The Taylor series indicates that $-J_1(x)$ is the derivative of $J_0(x)$, much like $-\sin(x)$ is the derivative of $\cos(x)$; more generally, the derivative of $J_n(x)$ can be expressed in terms of $J_n\pm 1(x)$ by the identities below [7].
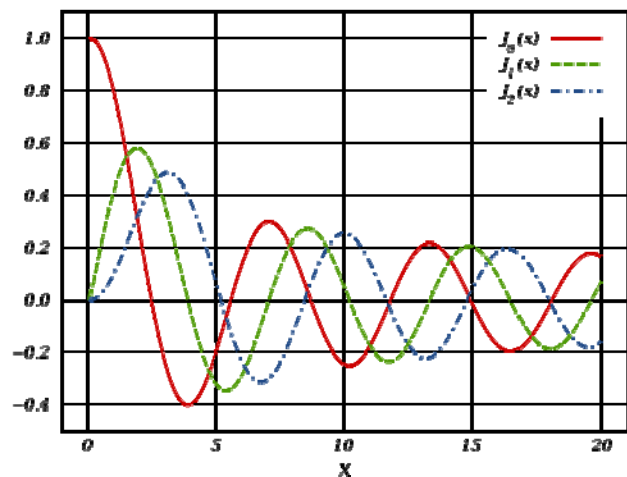

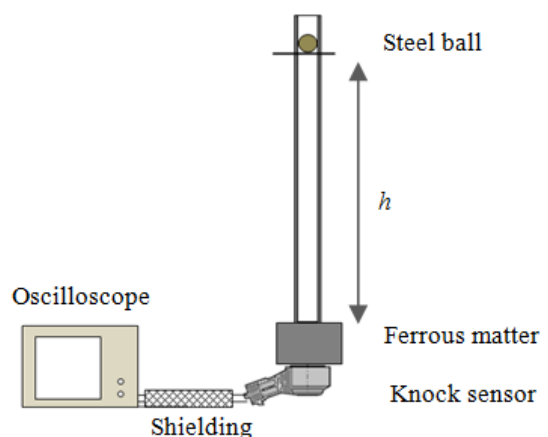Fig. 4. Plot of Bessel function of the first kind, $J_a(x)$ [6]

Fig.5. Testing device

A simple but effective test knock sensor is shown on Fig.5. The sensor is attached to a metal cylindrical body. The plastic tube is adjusted so as to allow for the impact of the metal balls of different heights h.

Impact of ball on a metallic material with a height of 1.8 cm and a diameter of 3.4 cm generates sound waves. These waves are captured by a knock sensor. The output voltage signal, which is shown in Fig.6, corresponds with Bessel function.

Using a measuring apparatus consisting of an oscilloscope, metal impact surface, plastic tube with adjustable height and metal ball, we tested the response the knock sensor from Bosch which was used in VW Golf. The response was stored in oscilloscope and then the values of voltage was shown in Fig.6.
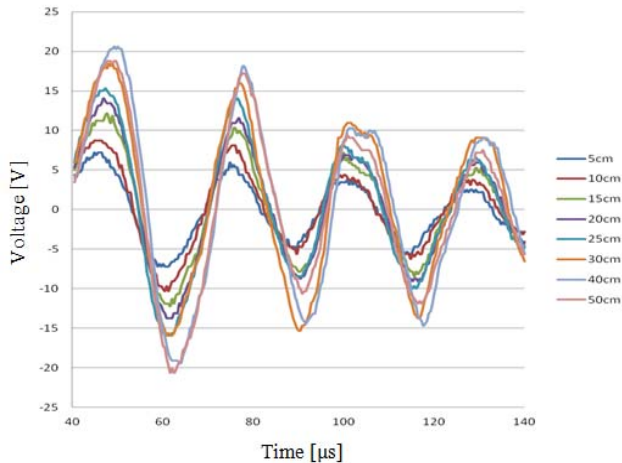

Fig.6. Output voltage of the sensor

The principally schematic of sound waves spreading in metal environment created by ball impact on surface of metal material is shown in Fig.7. The knock sensor is placed on the bottom of the metal plate. In the middle of the plate is screw which is tighten to rated torque. This arrangement provide the best possible transfer of mechanical waves on the surface of the sensor and
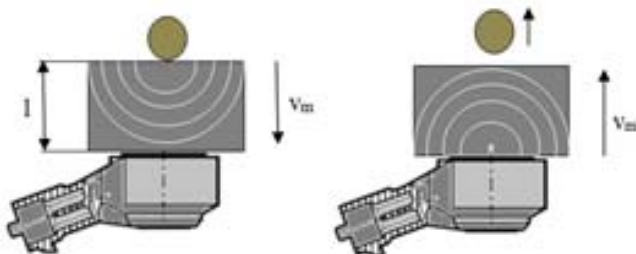

Fig.7. Sound reflection after the bullets' impact

The diagnostic of knock sensor is based on response of knock sensor on the first two extremes of the measured signal. The amplitude of signal is showed how this sensor is sensitive and how shape is sensor response. From measured values we could specify a "normal curve" which show how big should be the voltage response from this kind of sensor. It replaces the mounting used by the manufacturer for this sensor.

The value of the generated voltage depends on the gravitational potential energy of the falling bullet:

$$(7) \qquad E_p = m \cdot g \cdot h$$

where m is the mass of the body (2050 mg), g is the acceleration due to gravity (9.81 m/s^2), h is the height of the body above the surface (5 cm, 10 cm, 15 cm, 20 cm, 25 cm, 30 cm, 40 cm, 50 cm).

Calculation of the output voltage can be realized by means of the formula:

$$(8) \qquad U = 20 \cdot \log(E_p + 1).$$

Restriction reflecting the sound waves can be accomplished by changing the shape of a metallic material. An experiment was conducted where a steel ball was thrown directly at the sensor. In this impact we can already consider the Bessel function.
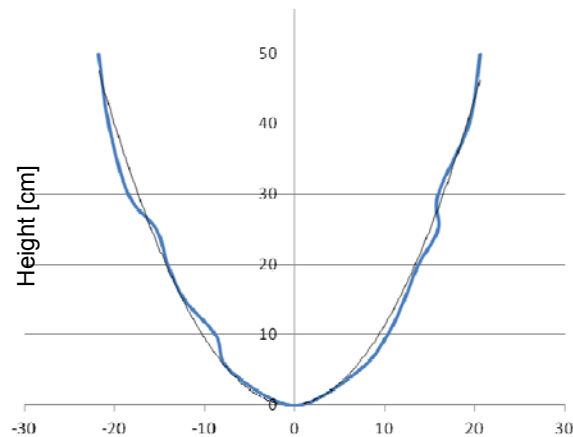

Fig. 8. Output voltage depending on the amount of the impact

Fig.9 shows the 3D model of knock sensor. It is modelled on materials composition and function like in real use. Cover of sensor is made from plastic and electrodes are made from metal. Inner pressure sensitive layer is simulated by crystal. On this model is affecting outer force. Model is detailed because the response of crystal is influenced by sensor cover and body of sensor too. Fig.10 shows knock sensor simulation in the COMSOL [8] at pressure of 1 N. In Fig.10 we can see an electric potential of the sensor.
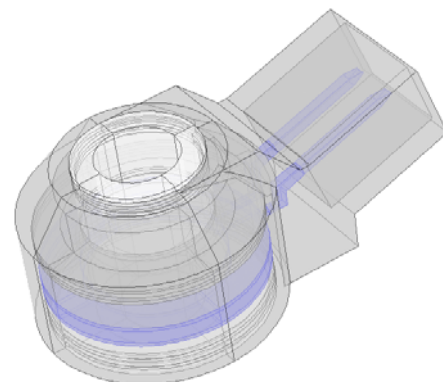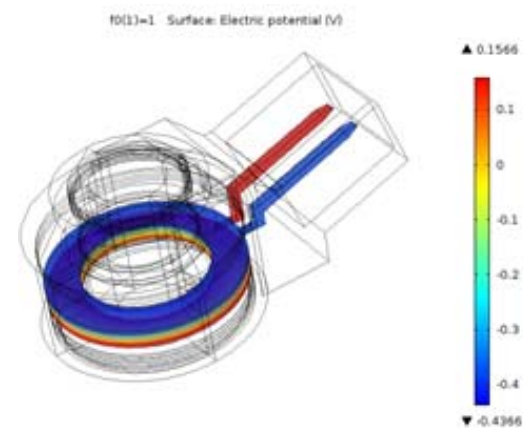

Fig.9. 3D model of knock sensor

Fig.10. Output potentials of sensor with 1 N of force affecting on piezoelectric element

Conclusion

A construction of the testing device for the knock sensor suitable for diagnostics of knock combustion in internal combustion engines has been presented.

The output signal of presented sensor has been described by Bessel functions. Using the first voltage extremes on the characteristics from Fig.6 it is possible to create a reference for the evaluation of the polynomial residue. It should be taken into account that the velocity of sound in air is 330 m/s. This sound impinges on the walls of the combustion chamber and is detected by the sensor. The resonant frequency of the clicking of the motor is usually in the range from 5 kHz to 15 kHz. The sensor worked in the field to 37 kHz, which shall be taken into account on an own sensor resonance.

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